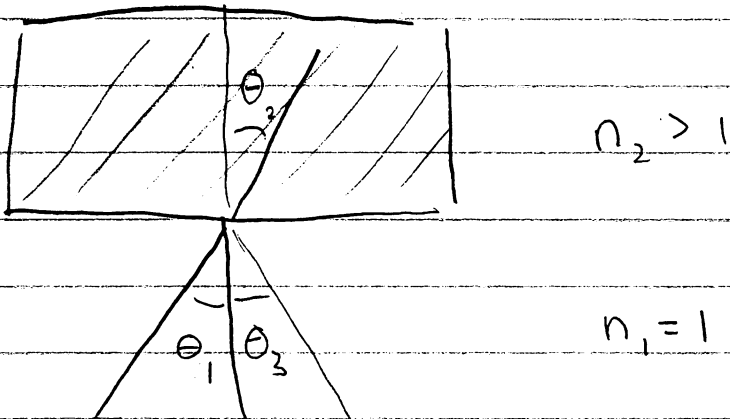


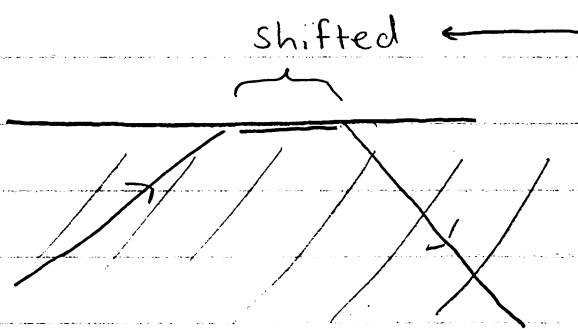
Reflection of Light at Interfaces - Introduction



Points to understand / derive :

- Snell's Law $n_1 \sin \theta_1 = n_2 \sin \theta_2$

- Internal Reflection



This is known as the Goos-Hänchen effect and is similar to tunnelling.

when $n_1/n_2 \sin \theta_1 > 1$

- Evaluate the forces on the interface, by evaluating the stress tensor

- How much light is reflected depends on the polarization of the incoming light.

Depending on whether the magnetic or electric field points out of the scattering plane, (Transverse Magnetic or Transverse Electric - see handout) more or less light is reflected.

Thus unpolarized light will be partially polarized upon reflection

This is used by radio towers to select transmitted light.

Transverse Magnetic

Region II

$$\mu_2 \epsilon_2$$

$$\mu_1 \epsilon_1$$

Region I

$$E_I$$

$$\theta_I$$

$$B_I$$

$$\odot$$

$$K_I$$

$$\theta_I$$

$$\theta_R$$

$$B_R$$

$$\odot$$

$$K_R$$

$$E_R$$

$$\theta_R$$

$$z$$

$$E_T$$

$$\theta_T$$

$$B_T$$

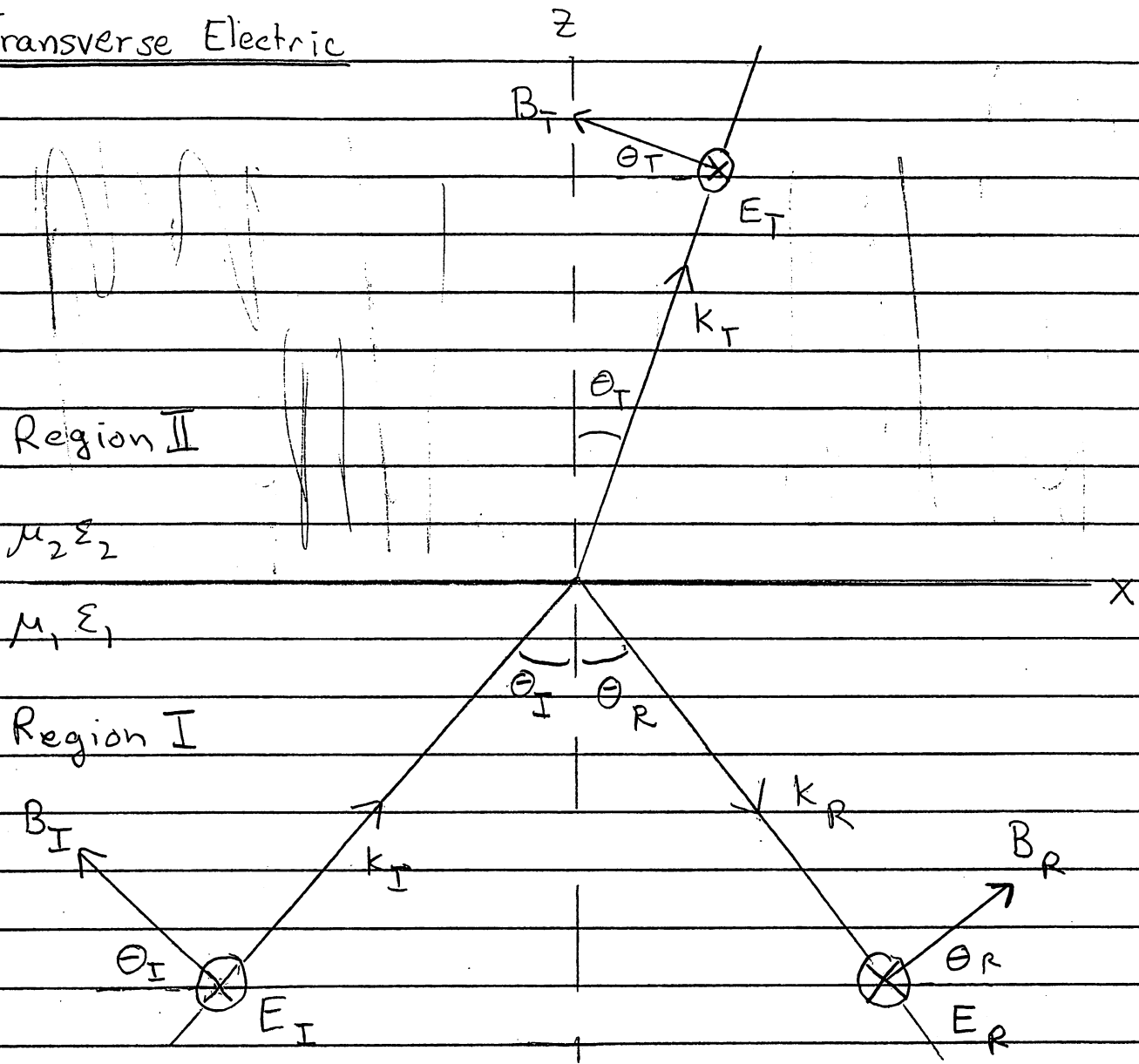
$$K_T$$

$$\theta_T$$

$$x$$

In this case the magnetic field points out of the scattering plane.

Transverse Electric



The transverse electric case is the magnetic dual of the transverse magnetic case

$$E \rightarrow B$$

$$B \rightarrow -E$$

The E -field points into page (\perp to scattering plane)

We will study the Transverse Magnetic Case:

- Basic idea write the solution in region II and region I as plane waves (sum of), and use boundary conditions to relate the two regions

Region II

← polarization vector

$$\vec{E} = \vec{E}_T e^{i\vec{k}_T \cdot \vec{r} - i\omega t}$$

$$\vec{H} = H_T e^{i\vec{k}_T \cdot \vec{r} - i\omega t} (-\hat{y}) \leftarrow \text{out of page}$$

transverse magnetic case
see figure!

Region I

$$\vec{E}_I(t, \vec{r}) = \vec{E}_I e^{i\vec{k}_I \cdot \vec{r} - i\omega t} + \vec{E}_R e^{i\vec{k}_R \cdot \vec{r} - i\omega t}$$

$$\vec{H}_I(t, \vec{r}) = (H_I e^{i\vec{k}_I \cdot \vec{r} - i\omega t} + H_R e^{i\vec{k}_R \cdot \vec{r} - i\omega t}) (-\hat{y})$$

Boundary Conditions

$$\vec{n} \cdot (\vec{D}_2 - \vec{D}_1) = 0$$

$$\vec{n} \times (\vec{H}_2 - \vec{H}_1) = 0 \quad (\text{Parallel components of } H \text{ continuous})$$

$$\vec{n} \cdot (\vec{B}_2 - \vec{B}_1) = 0$$

$$\vec{n} \times (\vec{E}_2 - \vec{E}_1) = 0 \quad (\text{Parallel components of } E \text{ continuous})$$

Solving the B.C:

- Has to hold at all times and for every point on the interface

$$i\vec{k}_I \cdot \vec{r} - i\omega t \Big|_{z=0} = i\vec{k}_R \cdot \vec{r} - i\omega t \Big|_{z=0} = i\vec{k}_T \cdot \vec{r} - i\omega t \Big|_{z=0}$$

- Frequencies, have to be the same, So:

$$k_I = |\vec{k}_I| = |\vec{k}_R| = \frac{\omega n_1}{c}$$

$$|\vec{k}_T| = \frac{\omega n_2}{c}$$

Thus the wavelengths are related $k_T = \frac{n_2}{n_1} k_I$

- At $z=0$, $\vec{k} \cdot \vec{r} \Big|_{z=0} = k_x x = k \sin \theta x$, so must have:

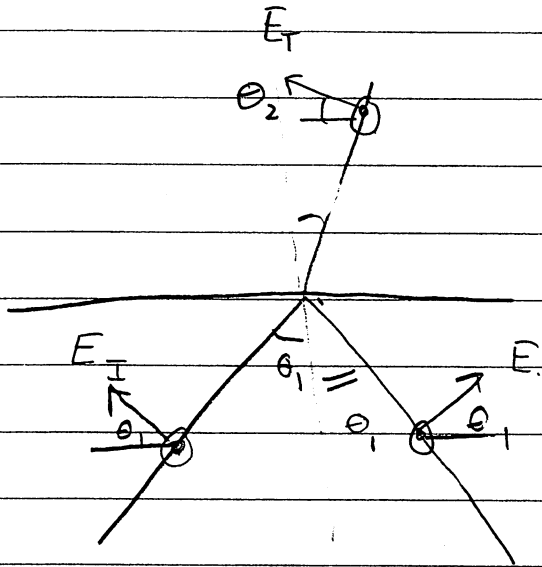
$$k_I \sin \theta_1 = k_R \sin \theta_3 = k_T \sin \theta_2$$

Or $\theta_1 = \theta_3$ incident = reflected

$$\sin \theta_1 = \frac{k_T}{k_I} \sin \theta_2$$

$$\sin \theta_1 = \frac{n_2}{n_1} \sin \theta_2 \quad (\text{snell's law})$$

Now E_{\parallel} continuous and H_{\parallel} continuous



So the x-components of E are continuous

$$-E_T \cos \theta_2 - (-E_I \cos \theta_1 + E_R \cos \theta_1) = 0$$

And from continuity of H

$$H_T - (H_I + H_R) = 0$$

So H is related to E , $H = E/z$

$$+\frac{E_T}{z_2} = (E_I + E_R)/z_1 = 0$$

+ Transmitted

Solving for the reflected amplitudes:

Find

$$\frac{E_R}{E_I} = \frac{Z_1 \cos \theta_1 - Z_2 \cos \theta_2}{Z_1 \cos \theta_1 + Z_2 \cos \theta_2} \Rightarrow \frac{Z_1 - Z_2}{Z_1 + Z_2}$$

head on

$$\frac{E_T}{E_I} = \frac{2Z_2 \cos \theta_1}{Z_1 \cos \theta_1 + Z_2 \cos \theta_2} \Rightarrow \frac{2Z_2}{Z_1 + Z_2}$$

head on

Now we want to analyze this:

• Energy Transport

$$\vec{S} = \frac{1}{2} c E \times H^* = \frac{c}{2} \frac{1}{Z} |E|^2 \hat{k}$$



time averaged poynting flux

So the transmitted power, relative to the input power:

$$\frac{T_P}{P} = \frac{\vec{S}_T \cdot \vec{n}}{\vec{S}_I \cdot \vec{n}} = \frac{\cos \theta_2}{\cos \theta_1} \frac{Z_1}{Z_2} \frac{|E_T|^2}{|E_I|^2}$$

$$\Rightarrow \frac{4Z_1 Z_2}{(Z_1 + Z_2)^2}$$

head on

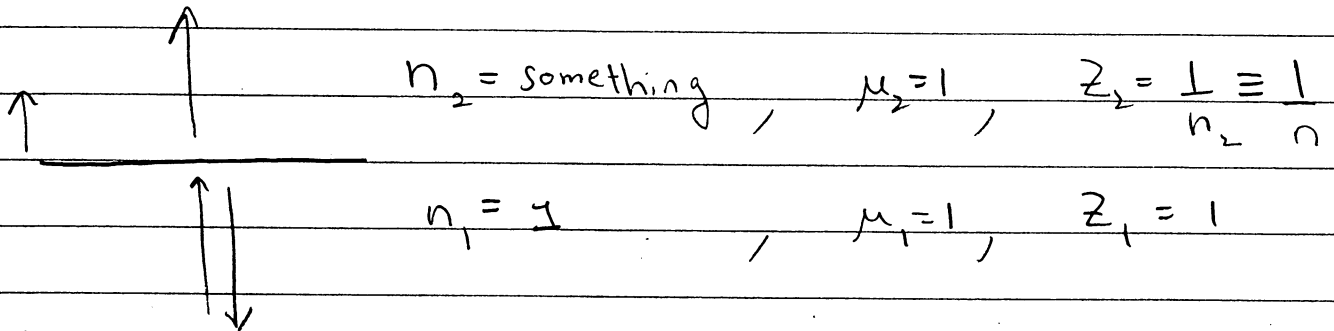
$$R_P = \frac{\vec{S}_R \cdot (-\vec{n})}{\vec{S}_I \cdot \vec{n}} = \frac{\cos \theta_1}{\cos \theta_1} \frac{Z_1}{Z_1} \frac{|E_R|^2}{|E_I|^2} \Rightarrow \frac{(Z_1 - Z_2)^2}{(Z_1 + Z_2)^2}$$

head on

Find generally

$$R_p + T_p = 1$$

Momentum Transport:



$$\frac{\text{Force}}{\text{Area}} = - (T_{out}^{zz} - T_{in}^{zz})$$

$$H = E/Z$$

$$T^{zz} = \frac{\epsilon}{2} (-E^z E^{z*} + \frac{1}{2} E \cdot E^* \delta^{zz}) + \frac{\mu}{2} (-H^z H^{z*} + \frac{1}{2} H \cdot H^* \delta^{zz})$$

time
ave

$$= \frac{\epsilon}{4} |E|^2 + \frac{\mu}{4} \frac{1}{\mu/\epsilon} E \cdot E^* = \frac{\epsilon}{2} E \cdot E^*$$

S_0

$$T_{out}^{zz} = \frac{\epsilon}{2} E_T^2 = \frac{\epsilon_1 \epsilon_2}{2} \left(\frac{\epsilon_2}{\epsilon_1} \left| \frac{E_T}{E_I} \right|^2 \right)$$

$$= \langle u_I \rangle (n T_p)$$

↑ incident energy density =
← transmission coefficient

index of refraction

Similarly

$$T_{in}^{zz} = \frac{\epsilon}{2} (E_I + E_R) \cdot (E_I + E_R)^*$$

$$T_{in}^{zz} = \frac{1}{2} \underbrace{E_I E_I^*}_{\langle u_I \rangle} (1 + R_p)$$

Find

$$\left\langle \frac{\text{Force}}{\text{Area}} \right\rangle = \langle u_I \rangle \left[1 + R_p - n T_p \right]$$

So for $\mu \approx 1$ and $n = 1/2$

$$\left\langle \frac{\text{Force}}{\text{Area}} \right\rangle = \langle u_I \rangle \frac{2(n-1)}{n+1} \xrightarrow{n \rightarrow \infty} 2 \langle u_I \rangle$$

Note:

↑ Total reflection

$$\langle u_I \rangle = c \langle g_{em} \rangle = \frac{\langle S \rangle}{c}$$

↑ energy density ≈ $\frac{m}{s}$ ↑ momentum / vol ↑ $\frac{\text{Energy}}{\text{Area} \cdot \text{time}} \cdot \frac{1}{m/s}$