

Last Time

$$-\square \varphi = \rho$$

$$-\square \vec{A} = \vec{J} / c$$

Then knowing the Grn-fcn of the wave-eqn.

$$\text{exact} \begin{cases} \varphi = \int_{r_0} \frac{\rho(T, r_0)}{4\pi |\vec{r} - \vec{r}_0|} \\ \vec{A} = \int_r \frac{\vec{J}(T, r_0) / c}{4\pi |\vec{r} - \vec{r}_0|} \end{cases} \quad T = t - \frac{|\vec{r} - \vec{r}_0|}{c}$$

Last time we considered the exact fields of a magnetic dipole. And we saw the transition from near field (see Sec

$$B(t, r) = \frac{3\vec{n}(\vec{n} \cdot \dot{\vec{m}}) - \dot{\vec{m}}}{4\pi r^3} \quad \left| \quad \text{(near field)} \right.$$

$T \leftarrow$ time

To far field

$$B(t, r) = \frac{-1}{4\pi r c^2} (\ddot{\vec{m}} - \vec{n}(\vec{n} \cdot \ddot{\vec{m}})) \quad \left| \quad \text{(far field)} \right.$$

\uparrow

powers of $\frac{1}{r}$ of near field (quasi-static)

result replaced with $\frac{1}{c} \frac{\partial}{\partial t}$

If all we care about is the far field
we have $T \approx t - r/c + n \cdot r_0/c$

$$\varphi = \frac{1}{4\pi r} \int_{r_0} \rho \left(t - \frac{r}{c} + \frac{n \cdot r_0}{c}, r_0 \right)$$

$$\vec{A} = \frac{1}{4\pi r} \int_{r_0} \frac{\vec{J}}{c} \left(t - \frac{r}{c} + \frac{n \cdot \vec{r}_0}{c}, \vec{r}_0 \right) \Leftarrow \text{All you need}$$

Then we expanded J and interpreted the result

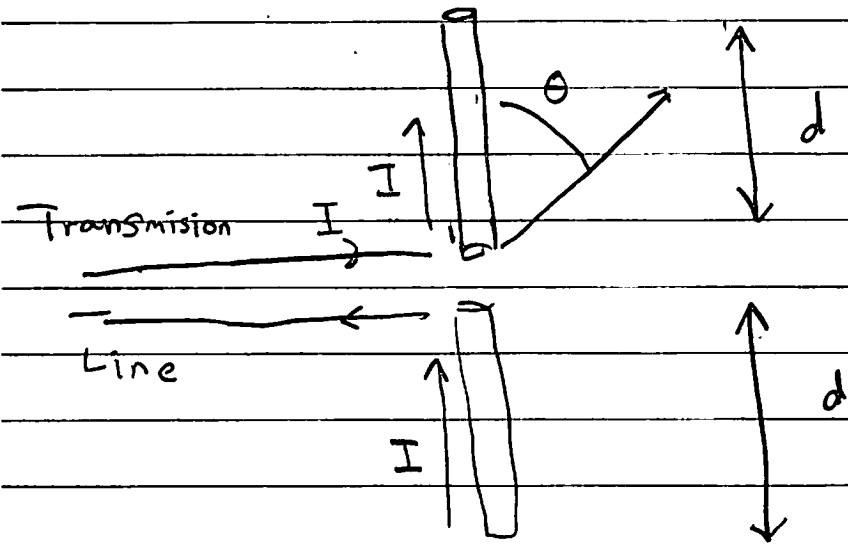
$$J \left(t - \frac{r}{c} + \frac{n \cdot \vec{r}_0}{c} \right) \approx J \left(t - \frac{r}{c} \right) + \frac{n \cdot r_0}{c} \dot{J} \left(t - \frac{r}{c} \right)$$

\nearrow \uparrow
e-dipole \quad m-dipole + e-quad.

Today

- Radio - Antennas
- Frequency spectrum for general currents

Linear Antennas (Center-Fed)



- The current goes to zero at the end
- Take a sinusoidal current

$$\vec{J}(t_0, \vec{r}_0) = I_0 \underbrace{\sin(kd - k|z_0|)}_{\text{Standing wave of current}} \hat{z} \delta(x) \delta(y) e^{-i\omega t_0}$$

$k = \omega/c$

Then

$$T = t - \frac{r}{c} + \frac{r_0}{c}$$

$$A(t, r) = \frac{1}{4\pi r} \int_{r_0} J(T, r_0) / c$$

$$= \frac{I_0}{4\pi r} e^{-i\omega(t-r/c)} \int_{-d}^d e^{-i\omega \frac{r-r_0}{c}} \sin(kd - k|z_0|) \hat{z} dz_0$$

Using $\frac{-i\omega n \cdot r_0}{c} = -ik z_0 \cos\theta$

$$\vec{A}(t, r) = \frac{I_0}{c} \frac{e^{-i\omega(t-r/c)}}{4\pi r} \hat{z} \int_{-d}^d e^{-ik z_0 \cos\theta} \sin(kd - k|z_0|) dz_0$$

$$= \frac{I_0}{c} \frac{e^{-i\omega(t-r/c)}}{4\pi r} \hat{z} \left[\frac{2}{k} \left(\frac{\cos(kd \cos\theta) - \cos(kd)}{\sin^2\theta} \right) \right]$$

So the power radiated

$$\frac{dP}{d\Omega} = c |r \ddot{\vec{E}}|^2$$

$$= c \left[r \left(\frac{-1}{c} \frac{\partial \vec{A}_T}{\partial t} \right) \right]^2$$

$$A_T = \vec{A} - \hat{n}(\hat{n} \cdot \vec{A})$$

$$\left(\frac{dP}{d\Omega} \right) = \frac{c}{2} \left[r^2 k^2 A_T(k) A_T^*(k) \right]$$

$$\frac{-1}{c} \frac{\partial A_T}{\partial t} = ik A_T$$

$$\overline{\frac{dP}{d\Omega}} = \frac{c}{8\pi^2} \left(\frac{I_0}{c} \right)^2 \left[\frac{\cos(kd \cos\theta) - \cos(kd)}{\sin\theta} \right]^2$$

Comments

① Previously we derived a multipole expansion valid when $kd \ll 1$, i.e. when

$$\frac{2\pi d}{\lambda} \ll 1$$

Thus when $kd \ll 1$ should recover the dipole limit. Indeed expanding for $kd \ll 1$

$$\frac{dP}{d\Omega} = \frac{c}{16\pi^2} \underbrace{\left(\frac{I_0}{c}\right)^2 (kd)^4 \sin^2 \theta}$$

See a characteristic dipole field and frequency dependence

② The total power can be determined

$$\bar{P} = \frac{1}{2} c \left(\frac{I_0}{c}\right)^2 \int \frac{d\Omega}{4\pi^2} \left[\frac{\cos(kd \cos \theta) - \cos(kd)}{\sin \theta} \right]^2$$

mks

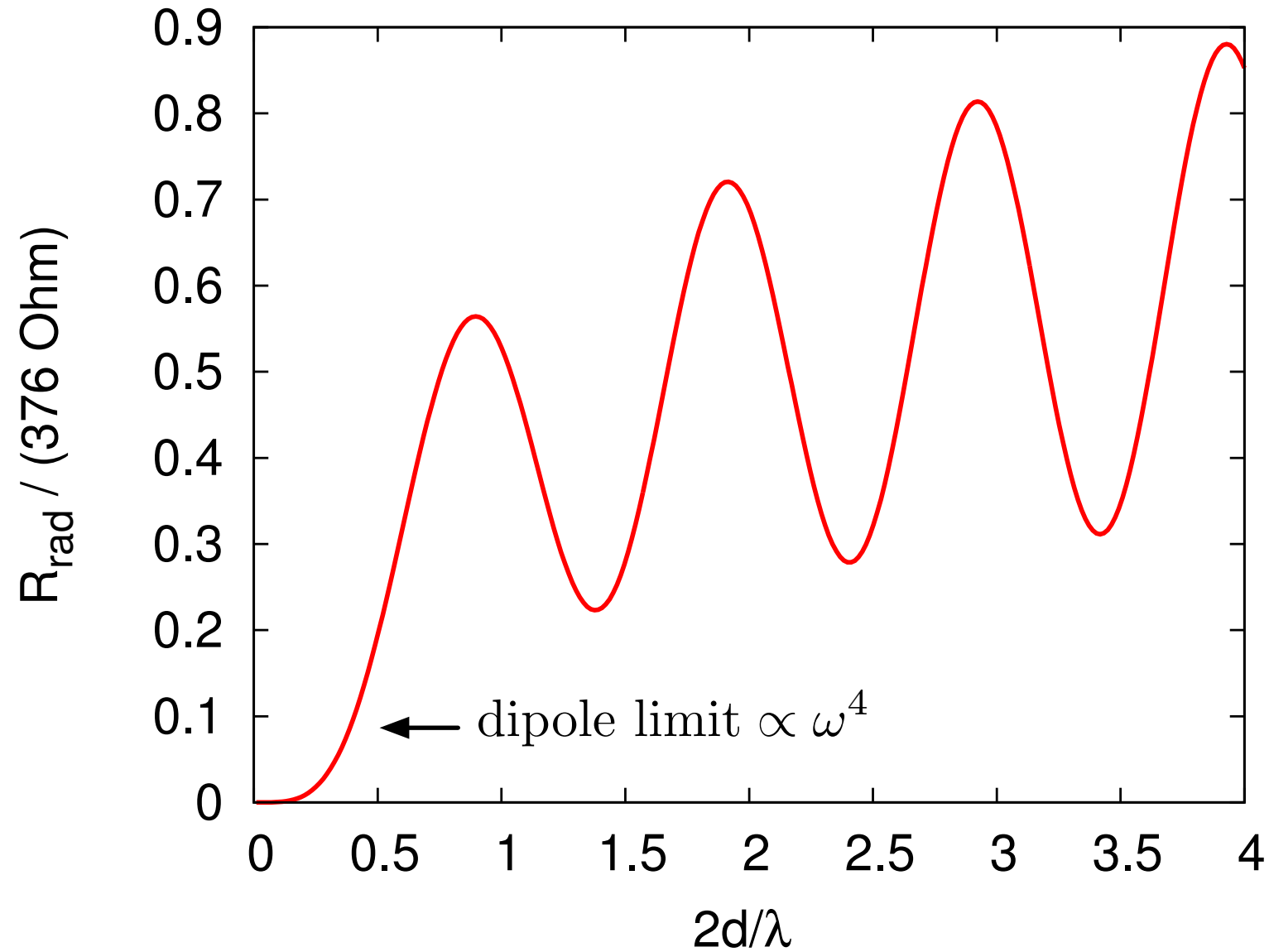
$$\bar{P} = \frac{1}{2} \underbrace{c \mu_0}_{\uparrow} I_{\text{mks}}^2 f(kd)$$

↑
have to do
numerically

this factor = $\sqrt{\frac{\mu_0}{\epsilon_0}}$ comes up all the time

and is the "Impedance of vacuum = 376Ω "

Radiation Resistance of an Antenna



Then can write.

$$P = \frac{1}{2} R_{\text{rad}} I_{\text{rms}}^2$$

Where the radiation resistance is

$$R_{\text{rad}} = 376 \Omega \int \frac{d\Omega}{4\pi^2} \left[\frac{\cos(kd \cos\theta) - \cos(kd)}{\sin\theta} \right]^2$$

Find numerically that

