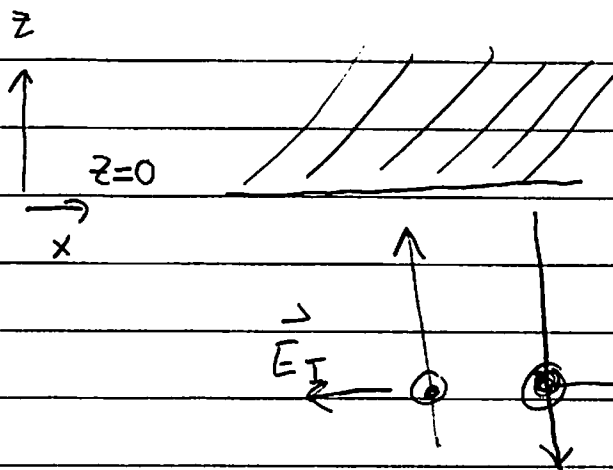


Reflection at Metal



• Metals are shiny.
Why?

• Basic reason: induced currents do not allow e^{-m} fields in metal

• At finite σ find corrections, wave penetrates a little

At $\sigma \rightarrow \infty$, find perfect reflection, \vec{E} vanishes at interface, i.e.

$$\vec{E}_R = -\vec{E}_I \quad \text{does the job}$$

So,

$$\vec{E}_I = \text{Re} \left[\vec{E}_I e^{ikz} + \vec{E}_R e^{-ikz} \right]$$

$$= 2\vec{E}_I \sin(kz)$$

← vanishes at interface

$$z=0$$

Find at finite σ , a small E_x and corresponding current

$$j_x = \sigma E_x$$

Maxwell Eqs in Metal

$$\nabla \cdot \vec{E} = \rho_{\text{mat}}$$

$$\nabla \times \vec{B} = \frac{\vec{j}}{c} + \frac{1}{c} \partial_t \vec{E}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{1}{c} \partial_t \vec{B}$$

no external
charges or currents

Then

$$\vec{j}_{\text{mat}} = \sigma \vec{E} + \chi_e \partial_t \vec{E} + c \chi_m^B \nabla \times \vec{B}$$

$$\begin{aligned} \vec{j}(\omega, \vec{x}) &= \sigma \vec{E}(\omega, \vec{x}) + (-i\omega \chi_e \vec{E}) + c \chi_m^B \nabla \times \vec{B} \\ &= (i\sigma/\omega + \chi_e) (-i\omega \vec{E}) + c \chi_m^B \nabla \times \vec{B} \end{aligned}$$

So from current consv.

$$\partial_t \rho = -\nabla \cdot \vec{j} \implies -i\omega \rho(\omega, \vec{x}) = -\nabla \cdot \vec{j}$$

Find

$$\rho(\omega, \vec{x}) = - \left(\frac{i\sigma}{\omega} + \chi_e \right) \nabla \cdot \vec{E} + \frac{c \chi_m^B}{-i\omega} \nabla \cdot (\nabla \times \vec{B})$$

So

$$\nabla \cdot \vec{E} = - \left(\frac{i\sigma}{\omega} + \chi_e \right) \nabla \cdot \vec{E}$$

Compare to
Dielectric

$$\underbrace{\left(1 + \chi_e + \frac{i\sigma}{\omega} \right)}_{\epsilon} \nabla \cdot \vec{E} = 0$$

Thus, $\left(\epsilon + \frac{i\sigma}{\omega} \right) \nabla \cdot \vec{E} = 0$

$$\epsilon \nabla \cdot \vec{E} = 0$$

Similarly

$$\nabla \times \vec{B} = \frac{1}{c} \frac{\partial \vec{E}}{\partial t} + \underbrace{\frac{1}{c} \partial_t \vec{E}}_{-i\omega \vec{E}}$$

$$\nabla \times \vec{B} = \frac{1}{c} \left(\frac{i\sigma}{\omega} + \underbrace{\chi_e + 1}_{=\epsilon} \right) (-i\omega \vec{E}) + \chi_m^B \nabla \times \vec{B}$$

So

$$\frac{1}{\mu} \nabla \times \vec{B} = \frac{1}{c} \left(\frac{i\sigma}{\omega} + \epsilon \right) (-i\omega \vec{E})$$

with $\mu = 1 / (1 - \chi_m^B)$, so

Dielectric

$$\nabla \times \vec{B} = \frac{\mu}{c} \left(\frac{i\sigma}{\omega} + \epsilon \right) (-i\omega \vec{E})$$

$$\nabla \times \vec{B} = \frac{\mu \epsilon}{c} (-i\omega \vec{E})$$

Thus conclude

The maxwell eqs are the same with the replacement

$$\epsilon \longrightarrow \hat{\epsilon}(\omega) = \epsilon + i\sigma/\omega$$

i.e

$$\hat{\epsilon} \nabla \cdot \vec{E} = 0$$

$$\nabla \times \vec{B} = \mu \frac{\hat{\epsilon}}{c} (-i\omega \vec{E})$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = i\omega \frac{\vec{B}}{c}$$

Note: that $\sigma \sim 10^{18} \text{ 1/s}$ $\omega \sim \text{GHz}$ so

$\frac{\sigma}{\omega} \gg 1$, while $\epsilon \sim 1$ thus

to a good approximation $\hat{\epsilon}(\omega) \approx \frac{i\sigma}{\omega}$

Wave-Solutions in Metal

- Try a solution $\vec{H}(\vec{x}) = \vec{H}_T e^{i\vec{k}\cdot\vec{x}}$ in Helmholtz eqn

$$\left(\nabla^2 + \omega^2 \frac{\mu \hat{\epsilon}}{c^2} \right) \vec{H}(\vec{x}) = 0$$

So

$$-k^2 + \omega^2 \frac{\mu}{c} \left(\frac{i\sigma}{\omega} \right) = 0$$

Find

$$k = \pm \sqrt{\frac{\omega \mu \sigma}{c^2}} \sqrt{i} = \sqrt{\frac{\omega \mu \sigma}{2c^2}} (1+i)$$

i.e

$$k = \pm \left(\frac{1+i}{\delta} \right)$$

$$\delta = \left(\frac{2c^2}{\omega \mu \sigma} \right)^{1/2}$$

So find then (selecting + sign for decreasing exponent)

$$\vec{H}(\vec{x}) = \vec{H}_T e^{-z/\delta} e^{iz/\delta} = \text{Re } \vec{H}_T e^{i\vec{k}\cdot\vec{x}}$$

Now lets look at $\vec{E} \equiv \vec{E}_T e^{i\vec{k}\cdot\vec{x}}$

$$\nabla \times \vec{H} = \frac{\sigma \vec{E}}{c}$$

$$\text{or } i\vec{k} \times \vec{H} = \frac{\sigma}{c} \vec{E} \Rightarrow i \frac{(1+i)}{\delta} \hat{n} \times \vec{H}_T = \frac{\sigma}{c} \vec{E}_T$$

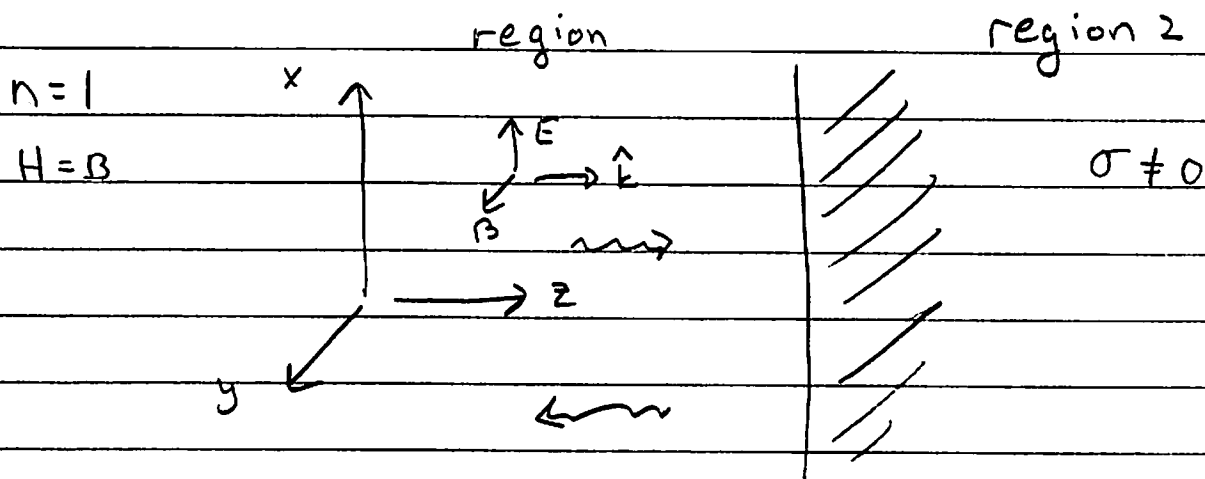
Thus with $\delta = \sqrt{\frac{2c^2}{\mu\omega\sigma}}$

$$\vec{E}_T = -\sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} \vec{n} \times \vec{H}_T$$

Note then that since $\sigma \gg \omega$,

we have $E \ll H$
in metal

Matching at the vacuum-metal interface



Region 1 - vacuum

$$\vec{E}_1 = (E_I e^{ikz} + E_R e^{-ikz}) \hat{x}$$

$$\vec{H}_1 = (H_I e^{ikz} + H_R e^{-ikz}) \hat{y}$$

given $\vec{E} = (-\hat{k}) \times \vec{H}$, $E_R = -H_R$

$$\vec{E}_1 = (H_I e^{ikz} - H_R e^{-ikz}) \hat{x}$$

Region 2

$$\vec{H}_2 = H_c e^{k_T z} \equiv H_c e^{-z/\delta} e^{i z/\delta} \hat{y}$$

$$E_2 = \sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} H_c e^{k_T z} \hat{x}$$

Matching

H_{\parallel} is continuous: $n \times (\vec{H}_{\text{out}} - \vec{H}_{\text{in}}) = 0$

$$(1) \quad H_c - (H_I + H_R) = 0$$

E_{\parallel} is continuous: $n \times (\vec{E}_{\text{out}} - \vec{E}_{\text{in}}) =$

$$(2) \quad \underbrace{\sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} H_c}_{E_c \ll H_c} - \underbrace{(H_I - H_R)}_{E_{\text{in vacuum}}} = 0$$

Small $\omega \ll \sigma$

Solve order by order (although you can do it exactly)

0th $H_I = H_R$ and $H_c = 2H_I$

so $E_I = H_I = H_R = -E_R$

find perfect reflector

since it multiplies $\sqrt{\frac{\omega}{\sigma}}$

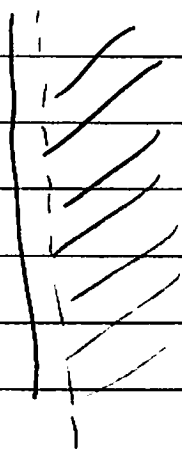
1st can use $H_c \approx 2H_I$ in Eq. (2) and solve for H_R

$$H_R = H_I - 2 \sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} H_I$$

Now Eq (1) gives

$$H_c = H_I + H_R = 2H_I - \underbrace{2 \sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} H_I}_{\text{small}}$$

Energy Flow into metal



Evaluate the Poynting flux just inside metal

$$\vec{S}_c \cdot \vec{n} \Big|_{z=0} = \frac{c}{2} \operatorname{Re} E \times H^* \quad \leftarrow \text{small}$$

$$H = H_c e^{i k_T z} \Big|_{z=0} = H_c = 2H_I + \text{small}$$

$$E = \operatorname{Re} \sqrt{\frac{\mu\omega}{\sigma}} \frac{(1-i)}{\sqrt{2}} H_c e^{i k_T z} \Big|_{z=0} = \sqrt{\frac{\mu\omega}{\sigma}} \frac{1}{\sqrt{2}} \cdot 2H_I$$

So

$$S_{\text{loss}} = \int \vec{e} \cdot \vec{n} = c \sqrt{\frac{\mu\omega}{\sigma}} \frac{2 \cdot 2}{2} \frac{1}{\sqrt{2}} H_I^2 \hat{z} \cdot \hat{z}$$
$$= c \sqrt{\frac{2\mu\omega}{\sigma}} |H_I|^2$$

The input energy is :

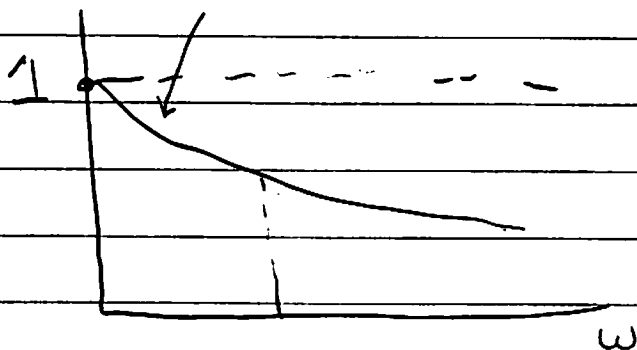
$$S_{\text{in}} = \frac{c}{2} |H_I|^2$$

So

$$R = \frac{S_{\text{in}} - S_{\text{loss}}}{S_{\text{in}}} = 1 - \frac{S_{\text{loss}}}{S_{\text{in}}}$$

$$R \approx 1 - 2 \sqrt{\frac{2\mu\omega}{\sigma}}$$

R describes the reflection coefficient here



Energy dissipated in Conductor - Direct Calculation pg. 1

$$\left\langle \frac{dW}{dt} \right\rangle_{\text{time ave}} = \int_V d^3x \frac{\text{Re}(\vec{j}^* \cdot \vec{E})}{2}$$

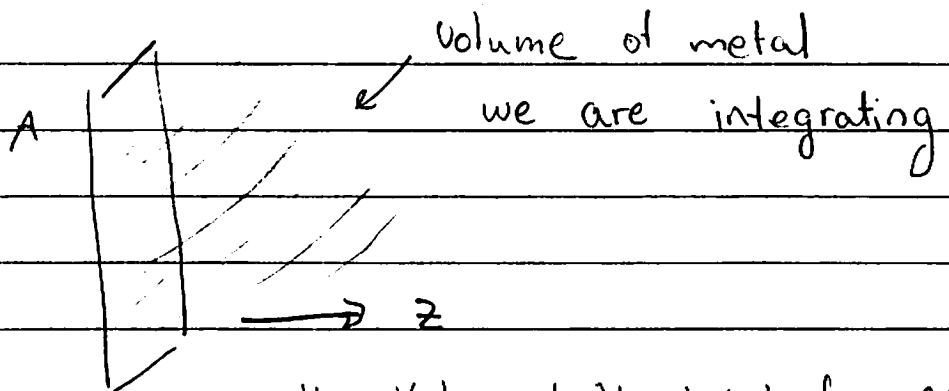
for a time ave
take half Re part

$$= \frac{1}{2} \sigma \int_V d^3x |E|^2$$

$j = \sigma E$

$$= \frac{1}{2} \sigma A \int_0^{\infty} dz |E|^2$$

area



Using H_c value of H at interface $\approx 2H_I$

$$|E_c|^2 = \frac{\mu\omega}{\sigma} |H_c|^2 e^{-2z/\delta}$$

do integral use $\delta = \sqrt{\frac{2c^2}{\mu\omega}}$

$$S_0 \left[\frac{1}{A} \left\langle \frac{dW}{dt} \right\rangle \right] = \frac{1}{2} \sigma \int_0^{\infty} dz \frac{\mu\omega}{\sigma} 4H_I^2 e^{-2z/\delta} = \left[\frac{c}{\sqrt{\frac{\mu\omega}{\sigma}}} 2\mu\omega |H_I|^2 \right]$$

This agrees @ S_{loss} the flux into metal.